

PATENT APPLICATION

ENTITLED:

METHOD FOR FORMING A MR READER WITH REDUCED SHIELD TOPOGRAPHY AND LOW PARASITIC RESISTANCE

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METHOD FOR FORMING A MR READER WITH REDUCED SHIELD TOPOGRAPHY AND LOW PARASITIC RESISTANCE

CROSS-REFERENCE TO RELATED APPLICATION(S)

5 This application claims the priority benefit of a provisional U.S. patent application serial number 60/322,311 of Dimitar V. Dimitrov, Daniel P. Burbank, Paul E. Anderson, Richard P. Larson, Kenneth P. Naughton, and Insik Jin, filed on September 12, 2001 and entitled "SV Reader Design With Reduced Shield Topography and Low Parasitic Resistance."

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BACKGROUND OF THE INVENTION

 The present invention relates to manufacturing of magnetoresistive spin valve (SV) devices. In particular, the present invention relates to a method of fabricating abutted junction SV heads for longitudinal recording.

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 A magnetic read head retrieves magnetically-encoded information that is stored on a magnetic medium or disc. The magnetic read head is typically formed of several layers that include a top shield, a bottom shield, and a read sensor positioned between the top and bottom shields. Also positioned between the top and bottom shields, abutting opposite sides of the read sensor, are biasing layers and current contacts. The read sensor is generally a type of magnetoresistive (MR) sensor. The resistance of the MR sensor fluctuates in response to a magnetic field emanating from a magnetic medium when the MR sensor is used in a magnetic read head and positioned near the magnetic medium. By providing a sense current through the MR sensor, the resistance of the MR sensor can be measured and used

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25 by external circuitry to decipher the information stored on the magnetic medium.

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 The spin valve effect is one known way to utilize magnetoresistance. Present abutted junction SV technology utilizes SV stacks with a thickness around 400 angstroms, while a combined thickness of surrounding biasing layers and current contacts is close to 1000 angstroms. This 600 angstrom difference in thickness creates a non-planar top shield topography near the sensor. For SV

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readers targeted at 100 kTPI and above, this top shield non-planar topography is comparable to the lateral dimensions of the reader. As a result, this non-planar topography presents serious concerns.

First, the top shield is made of soft magnetic material, which tends to break into magnetic domains in regions with corners and non-planar topography. Formation of magnetic domains in the top shield that are in close vicinity to the MR sensor is highly undesirable, because it is expected to be a source of magnetic instability and, thus, increase noise in the reader.

Second, the top and bottom shields need to shield the MR sensor from down-track transitions on the magnetic media and enable adequate electrical pulse-width (PW_{50}), which is the width of the pulse signal at 50% peak amplitude, of the MR read sensor. These are achieved when a spacing between the bottom shield and the top shield are at a minimum. Large top shield non-planar topography is expected to compromise the shield-to-shield spacing at the edges of the sensor, thus deteriorating the down-track shielding capability and the PW_{50} .

Third, the top and bottom shields need to shield the MR sensor from transitions in adjacent tracks on the magnetic media and provide adequate electrical reader width, which is evaluated by the MT_{50} and MT_{10} values. MT_{50} and MT_{10} values are the width of the pulse signal at 50% and 10% peak amplitude, respectively. Large top shield non-planar topography is expected to allow more flux penetration from the adjacent tracks. This will lead to deteriorated MT_{50}/MT_{10} values or, alternatively, would require narrower physical reader width to achieve the required electrical reader width.

The conventional method of fabricating MR readers first defines a reader width of the MR sensor and then defines a back edge of a stripe height of the MR sensor. As will be explained below, this process creates a region of significantly thinned current contacts behind the stripe height back edge. After lapping an air bearing surface (ABS) of the MR sensor to define a stripe height

front edge, the thickness of the remaining part of the current contacts is significantly reduced. Consequently, current supplied to the MR sensor through the current contacts is forced to go through two paths that have high resistance--one is a thick but narrow strip at the ABS, while the other is a wide but thin region extending
5 behind the stripe height back edge. This creates large parasitic resistance. While this large parasitic resistance is within acceptable values when the top shield non-planar topography is 600 angstroms (contacts plus biasing layers equal to 1000 angstroms), it will become very large if the contact thickness is reduced in order to create flat top shields (contact plus biasing layers equal to 400 angstroms).
10 Electronics associated with the MR reader are not optimized for these high resistance levels and redesigning the electronics would be too costly.

Therefore, there is a need for a method of fabricating a MR reader with top shield planar topography. Additionally, the method must be economical and minimize parasitic resistance.

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BRIEF SUMMARY OF THE INVENTION

The present invention is a method for fabricating a magnetoresistive reader having a sensor, current contacts with low parasitic resistance and a top shield with substantially planar topology. First, a stripe height back edge of the
20 sensor is defined, and second, a reader width of the sensor is defined. The current contacts are deposited to a thickness such that a top surface of the current contacts is substantially level with a top surface of the sensor. The top shield is deposited over the sensor and the current contacts. Defining the stripe height back edge prior to the reader width results in current contacts with low parasitic resistance and
25 allows for thin contacts and flat top shield, which inhibits the formation of magnetic domains in the top shield.

BRIEF DESCRIPTION OF THE DRAWINGS

Figures 1-5 illustrate steps in a conventional method for forming a MR reader.

Figures 6-9 illustrate steps in accord with the present invention for forming a MR reader.

Figures 10a and 10b are electrical potential distribution maps of a MR reader made by the conventional method.

Figures 11a and 11b are electrical potential distribution maps of a MR reader made by the method of the present invention.

Figure 12 is a graphical representation comparing a parasitic resistance contribution from the fabrication process (R_{mill}) to a mill window width (MW) used to fabricate MR readers.

Figure 13 is a graphical representation comparing R_{mill} to a stripe height of MR readers.

DETAILED DESCRIPTION

A sensor of an MR reader is formed by defining four critical edges: a front and back edge defining a stripe height of the sensor and side edges defining a width of the sensor (a reader width). Conventionally, the reader width is defined first, followed by definition of the stripe height back edge and then the stripe height front edge. Figures 1-5 illustrate steps in a conventional method of forming MR reader 10.

Figure 1 is a cross-sectional view of MR reader 10 in the process of having its reader width defined by the conventional method. MR reader 10 includes bottom shield 12, bottom half-gap 14, SV stack 16 having reader width 18, photoresist release layer (PMGI) or photoresist bridge 19, and first photoresist layer 20. Bottom shield 12 is deposited on a wafer (not shown) covered with an appropriate basecoat (Al_2O_3 layer) followed by bottom half-gap 14 and then SV

stack 16. Bottom half-gap 14 is an insulator that is usually made of Al_2O_3 . A specific pattern of first photoresist layer 20 is suspended over SV stack 16 using photoresist release layer (PMGI) or photoresist bridge 19. A width of first photoresist layer 20 adjacent to a desired SV sensor region of SV stack 16 defines reader width 18 of SV stack 16.

The purpose of first photoresist layer 20 is to mask regions during the milling process, which removes the material left unprotected. MR reader 10 with reader width 18 defined after the milling process is shown in Figure 1. At this point, two of the critical edges are defined: the side edges of reader width 18 of SV stack 16.

Figure 2 is a cross-sectional view of MR reader 10 illustrating another step in the conventional method of fabricating MR reader 10. This step involves depositing several layers in an abutting junction configuration adjacent opposite edges of SV stack 16. The specific components may vary, for example a pedestal may be included. In the embodiment shown, permanent magnet seed 22 is deposited, then permanent magnet 24, followed by extended contacts 26. Next, first photoresist layer 20 is dissolved (not shown).

Figure 3 is a top view of MR reader 10 showing MR reader 10 masked for defining stripe height back edge 30. Second photoresist layer 28 masks part of SV stack 16 and contacts 26 but leaves open the area behind desired stripe height back edge 30, which is defined. Stripe height back edge 30 is protected by backfilling the milled area with Al_2O_3 or other suitable material, and second photoresist layer 28 is subsequently dissolved. The last step involves defining the final critical edge, which is the front edge of the stripe height. Lapping MR reader 10 at the front edge defines the stripe height front edge (or the ABS).

Figure 4 is a top view of MR reader 10 schematically showing MR reader 10 with defined sensor 32. After lapping the ABS of MR reader 10, sensor 32 is fully defined having reader width 18 and stripe height 36. The second milling

process has cleared the exposed SV stack 16 and contacts 26. Bottom half-gap 14 is exposed from underneath SV stack 16. Exposed contacts 26 have been milled to a very minimal thickness represented by milled contacts 38. Contacts 26 now form a thick but narrow region near sensor 32. This configuration leads to large parasitic resistance as current is directed toward sensor 32. The current is forced through contact paths that are thick but narrow (contacts 26) and wide but thin (milled contacts 38).

Figure 5 is a cross-sectional view of finished SV reader 10. Here, top half-gap 40 has been deposited over contacts 26, milled contacts 38 (not shown), and SV stack 16. Top shield 42 is then deposited over top half-gap 40.

As shown schematically, because of the non-planar topography where contacts 26 abut SV stack 16, top shield 42 also has non-planar topography. As previously discussed, this leads to magnetic domains forming in top shield 42 that may interfere with the signal generated by SV reader 10.

One approach to reduce top shield 42 non-planar topography is to use two sets of contacts: a first set that matches SV stack 16 thickness and extends out from sensor 32, and a second set that is much thicker and recessed from sensor 32. With this approach, the non-planar topography of top shield 42 is moved away from sensor 32.

This alternate approach, however, presents two major drawbacks. First, a large increase in resistance is expected, which poses issues for the associated electronics and may increase Johnson noise in the MR reader. Second, the approach requires a second set of contacts which increases the process content, adds to the fabrication cost, and potentially increases the chances for problems that lead to scrapping wafers.

In order to create planar topography in the vicinity of the sensor, it is necessary to thin the current contacts to approximately the SV stack thickness. If reader width 18 definition is performed before stripe height 36 definition, the mill

operation to define stripe height back edge 30 will decrease the thickness of the contacts behind the line of back edge 30. The result is a narrow and long strip with large parasitic resistance contribution in series with sensor 32, and the parasitic contribution has very strong dependence on stripe height 36.

5 The method of the present invention illustrated in the Figures 6-9 alleviates the problems associated with the previously described conventional techniques. The process begins, as with the conventional method, by depositing bottom shield 12, bottom half-gap 14, and SV stack 16. Figure 6, which is a top view of MR reader 10, illustrates the step of defining stripe height back edge 30. Figure 6 shows second photoresist layer 28 selectively patterned on SV stack 16, leaving exposed a region of SV stack 16 behind desired stripe height back edge 30 to define stripe height back edge 30. MR reader 50 is milled and bottom half-gap 14 is revealed in the unprotected region. Thus, the first critical edge, stripe height back edge 30, is defined.

15 Stripe height back edge 30 is backfilled to protect edge 30 and second photoresist layer 28 is subsequently dissolved. Preferably the backfill is Al_3O_2 , and has a thickness that leaves enough insulation after the milling process to define reader width 18. To enable the reader width bridge process, which suspends first photoresist layer 20 over SV stack 16 in the region where sensor 32 will be, the backfill should be at about the same level as SV stack 16.

20 Figure 7 shows the next step in the process, which is defining reader width 18. Figure 7 shows MR reader 50 with first photoresist layer 20; bottom half-gap 14, which was exposed in the previous mill process; and SV stack 16 with stripe height back edge 30, which was masked in the previous step. Again, first photoresist layer 20 serves to define reader width 18 of MR reader 50.

25 After selective placement of first photoresist layer 20, MR reader 50 is milled again to remove an unprotected region of SV stack 16. Second photoresist layer 20 remains while contacts 26 are deposited such that a top surface of SV stack

16 extends at a same level as a top surface of contacts 26. Preferably, other materials are deposited prior to contacts 26. These materials may include a pedestal layer, permanent magnet seed, and permanent magnet. Second photoresist layer 20 is subsequently dissolved. Reader width 18 is now defined.

5 To finish MR reader 50, top half-gap 40 is deposited and then top shield 42 is deposited. Stripe height front edge 34 is defined, as in the conventional method, by lapping the ABS of MR reader 50 to finalize definition of all critical edges of sensor 32.

10 Figures 8 and 9 show finished MR reader 50. Figure 8 is a top view without top gap 40 or top shield 42, while Figure 9 is a cross-sectional, ABS view of finished SV reader 50. SV reader 50 includes bottom shield 12, bottom gap 14, sensor 32 having reader width 18 and stripe height 36 defined by back and front edges 30 and 34, respectively; permanent magnet seed 22; permanent magnets 24; current contacts 26; top gap 40; and top shield 42. Using the method taught here,
15 contacts 26 have uniform thickness throughout. The wide layer forming contacts 26 has reasonably large (about 400 angstroms) thickness and decreased parasitic resistance to acceptable levels. Additionally, top shield 42 exhibits planar topography since contacts 26 and SV stack 16 have planar topography. The problem of magnetic domains forming and interfering with sensor 32 is reduced
20 because of this planar topography of top shield 42. In addition, only one set of contacts 26 are used, which decreases process time, cost, and scrapped wafers.

 Finite element method (FEM) modeling was performed to study the parasitic resistance contribution from the milling process that defines stripe height 36 (Rmill). A SV reader fabricated using the conventional method was compared
25 to a SV reader fabricated using the method of the present invention. In all cases, a top surface of contacts 26 was assumed to be substantially level with a top surface of SV stack 16, which is 400 angstroms. A width of a mill window in photoresist layer 28 (MW), which defines stripe height back edge 30, is a major factor in

determining R_{mill} in the conventional method. Therefore, three different widths were tested: 0.55 μm , 0.75 μm , and 1.0 μm . MW can not be reduced to an arbitrarily low value because of limitations in achieving a straight stripe height back edge 30. Using the best DUV photo process presently available, the minimum width is 0.55 μm . Current 30 Gb/inch² to 50 Gb/inch² products use a 1.0 μm width. The examples studied all utilized Rhodium (Rh) or Gold (Au) pedestals, but the pedestals may be formed of other conductive material. Additionally, the SV reader can be formed without pedestals as illustrated above in Figures 6-9.

Figures 10a and 10b show the electrical potential distribution map of a SV reader fabricated using the conventional method with a Rh pedestal and MW of 0.55 μm . Figure 10b is an enlarged view of active sensor 32 illustrated in Figure 10a. Since contacts 26 are thinned by the milling process, current is squeezed through a narrow strip at the ABS causing a large parasitic resistance.

Figures 11a and 11b are analogous electrical potential distributions of a SV reader fabricated using the method of the present invention. Figure 11b is an enlarged view of active sensor 32 illustrated in Figure 11a. The current is not constrained so drastically, and this insures much lower R_{mill} . In fact, MW is irrelevant in this case, thus allowing MW to be optimized using other process constraints such as straightness of stripe height back edge 30, shadowing during milling, stripe height back edge 30 backfill process, and photoresist liftoffs.

To demonstrate the advantage of using the method of the present invention, R_{mill} was calculated for a number of cases. The results are presented in Figure 12. Stripe height 36 is assumed to be 400 angstroms, which is close to the target value for programs between 120-140 kTPI. When using the conventional method and a Rh pedestal, the minimum R_{mill} is 107 Ω and with an Au pedestal, the minimum R_{mill} is 70 Ω . Even the smaller 70 Ω value is much larger than the values of R_{mill} presently used, which are about 20-30 Ω and will render head resistances of 115 Ω for Au and 150 Ω for Rh pedestals.

However, in cases using the method of the present invention, significant improvements are seen. If a Rh pedestal is used, the R_{mill} is 38 Ω . If an Au pedestal is used, the R_{mill} is 25 Ω which is well within the range used in present technology.

5 Another advantage is illustrated in Figure 13. Figure 13 shows the results of comparing R_{mill} as a function of stripe height 36. Here, the pedestals are formed of Rh and MW is 0.75 μm . Using the conventional method to form the SV reader results in a strong inverse correspondence between R_{mill} and stripe height 36. This naturally leads to a wide distribution in head resistance if using a lap to stripe height slider process or lap to resistance slider process to define stripe height
10 front edge 34. Presently, the lapping processes produce significant variations in stripe height 36. The large variation in head resistance, as well as the large value itself, is not optimal for the design of the associated electronics.

 Conversely, when using the method of the present invention to
15 fabricate the SV reader, R_{mill} has little dependence on stripe height 36. Unlike when using the conventional method, typical variations in stripe height 36 do not substantially change the geometry of contacts 26. Regardless of stripe height, the current still passes through the same wide region and, thus, the small stripe height 36 dependence. In the conventional method, the resulting area that the current
20 passes through is a narrow, long strip along the ABS, and the typical variations in stripe height 36 will strongly affect resistance.

 Although the present invention has been described with reference to SV readers, the method of the present invention applies equally to other types of current in plane (CIP) MR readers, including AMR readers.

25 Although the present invention has been described with reference to preferred embodiments, workers skilled in the art will recognize that changes may be made in form and detail without departing from the spirit and scope of the invention.